

## Phase Transformations in Nitinol and Challenges for Numerical Modeling

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## Acknowledgments

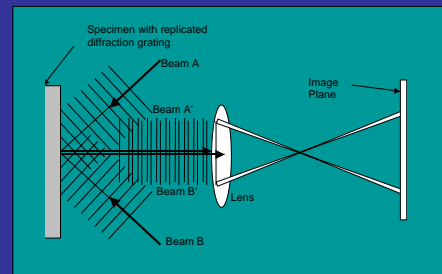
- Idaho National Engineering and Environmental Laboratory (INEEL)
  - Eric Steffler, Randy Lloyd, Keith Rozenburg, Dave Nielson, Vance Deason, Neal Boyce, Tom Walters, and Jo



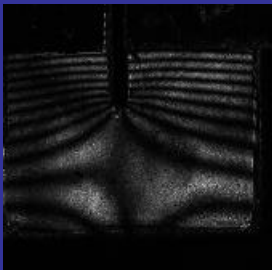
## Overview

- Motivation
  - Understand the mechanics of phase transformations in Nitinol
  - Improve engineering design and verification methods
- Moiré interferometry
- Results
  - Uniaxial tensile specimens
  - Compact tension specimens
  - (Four-point bend specimen)

## Moiré Interferometry



## Typical Moiré interferometry fringe pattern horizontal displacement field



$$\text{Intensity} = A + B \cos(f)$$

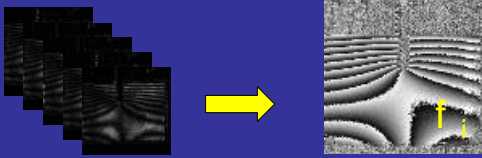
## Phase-Shifted Moiré Interferometry

- Four-beam fiber optic interferometer
- Variable frequency adjustable (120–1200 1/mm gratings)



- Phase-shifted moiré (Perry, 1993)
  - Enhanced noise reduction
  - Preserves fine spatial resolution
  - Automated fringe processing
- Photoresist diffraction gratings
  - Spin coated resist
  - Ronchi ruling exposure
- Optical filtering at multiple diffraction and image planes

## Phase Shifting and Unwrapping



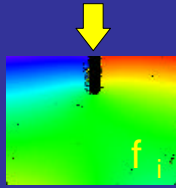
$$I_{ij} = A_i + B_i \cos(f_i + d_j)$$

$A_i, B_i, f_i$ : data at each pixel

$d_j$ : phase shift

$i$ : 1024x1024 pixels

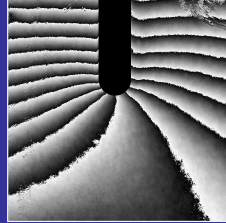
$j$ : 1 to 5 phase shifts



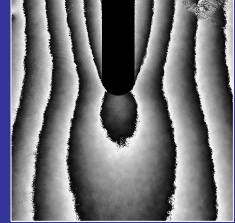
## Examples of Moiré fringe patterns

at low load prior to onset of SIM transformation

Horizontal displacement field

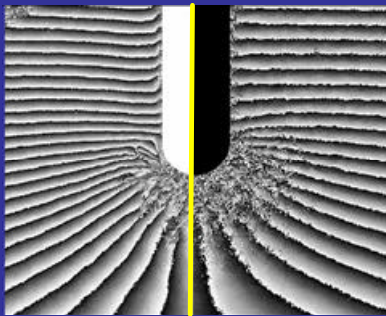


Vertical displacement field



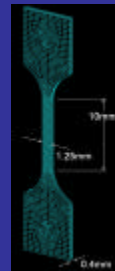
## Effect of specimen grating thickness

elevated load, near end of plateau



Moiré with epoxy grating    Moiré with photoresist grating

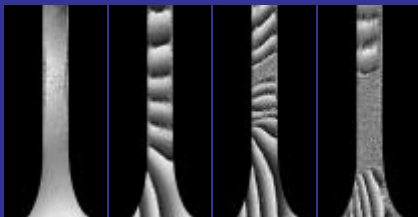
## Uniaxial tensile specimens



- Superelastic Nitinol
  - $A_i = -20^\circ\text{C}$  Material X
  - $A_i = -5^\circ\text{C}$  Material Y
- Two different processing histories
- Dimensions
  - Width 1.25 mm
  - Thickness 0.4 mm
  - Gage section 10mm

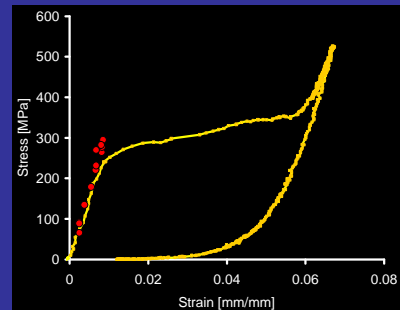
## Moiré Interferometry Results

progressive loading of uniaxial tensile specimens  
(Material X)



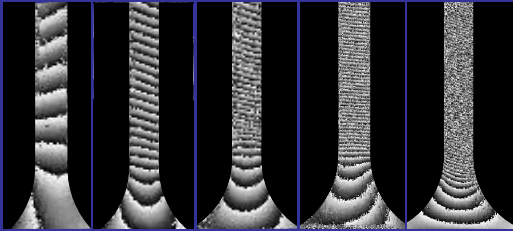
## Comparison of Global Data and Local Moiré Strain Measurements

(Material X)



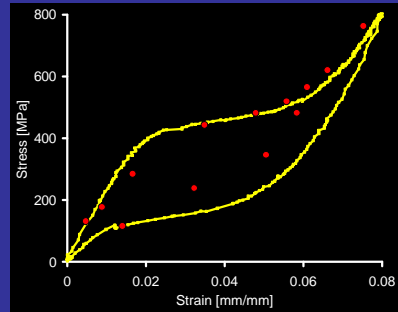
## Moiré Interferometry Results

progressive loading of uniaxial tensile specimens  
(Material Y)



## Comparison of Global Data and Local Moire Strain Measurements

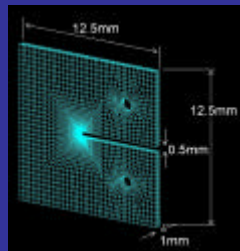
(Material Y)



## Compact tension specimens

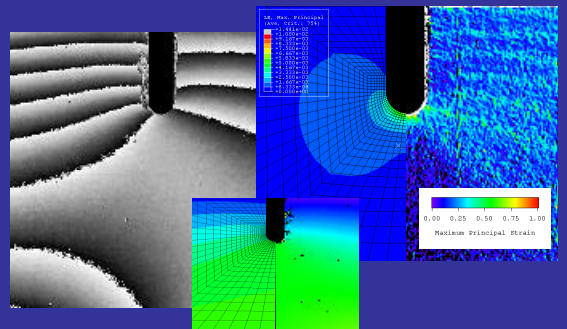
Compact Tension Samples

- Superelastic Nitinol,  $A_f = 25^\circ\text{C}$
- Longitudinal and transverse orientations
- Dimensions
  - Notch size  $500\ \mu\text{m}$
  - Thickness  $0.6\ \text{mm}$
  - Width  $12.54\ \text{mm}$



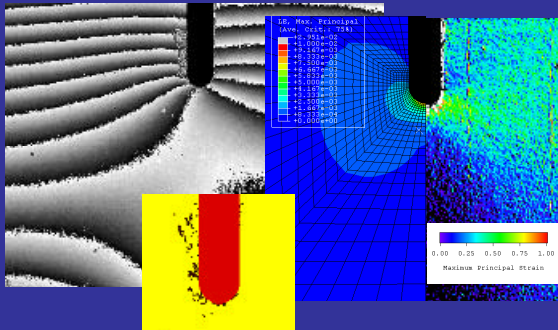
## Moiré Interferometry Results

low load, prior to SIM (30N)



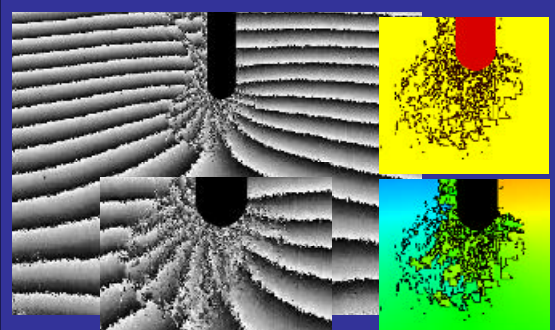
## Moiré Interferometry Results

intermediate load, near first evidence of SIM (199N)



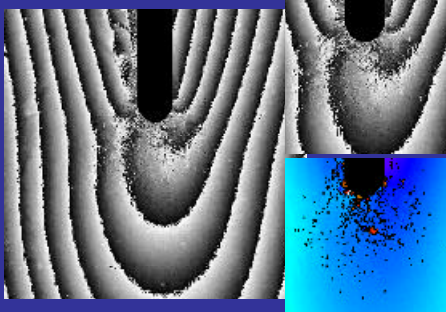
## Moiré Interferometry Results

partially unloaded (149N)



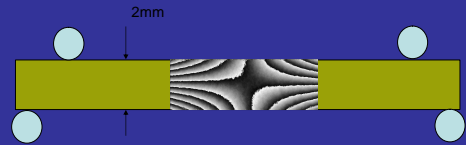
## Moiré Interferometry Results

partially unloaded (149N), vertical displacement field

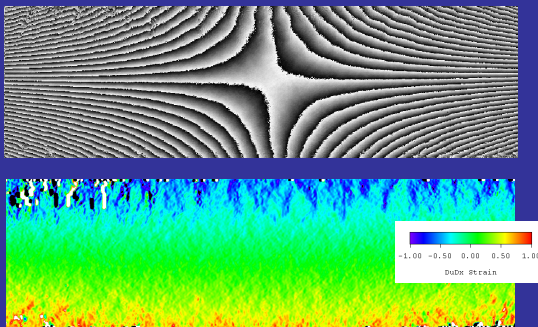


## Moiré Interferometry Results

four point bend experiment



## Moiré Interferometry Results



## Summary

- Phase transformation in Nitinol is sub grain size (<10microns) and distributed
- Lüders-type localization was seen in some uniaxial specimens, different behavior in other specimens
- Transformation around stress concentrations follows repeatable, distributed patterns
- Volume fraction of SIM increases with increasing load, even beyond the end of the plateau
- Elastic strain decreases in the transformation zone during unloading and SIM persists until near complete unloading
- No evidence of a SIM toughening mechanism, perhaps stress shielding and redistribution effects

## Conclusions

- Phase-shifted Moiré is an excellent technique for studying Nitinol and enables better engineering design and verification methods
- New material models should be developed which account for the observed distributed transformation behavior
- We still have more to learn